TubeTalker: An airway modulation model of human sound production

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Abstract
Artificial talkers and speech synthesis systems have long been used as a means of understanding both speech production and speech perception. This article begins with an overview and history of artificial speech systems which includes mechanical models, electronic devices, and computation-based simulations. The development of an airway modulation model is then described that simulates the time-varying changes of the glottis and vocal tract, as well as acoustic wave propagation, during speech production. The result is a type of artificial talker that can be used to study various aspects of how sound is generated by humans and how that sound is perceived by a listener. The primary components of the model are introduced and simulation of two phrases are demonstrated.

Keywords: vocal tract, vocal folds, modulation, speech synthesis.

1. Introduction
Humans have a system of airways that, for purposes of speech production, serves to transform articulatory movements into an acoustic wave that carries the distinctive characteristics of speech. This transformative process is accomplished by modulating the airway system on multiple time scales (cf. Fig. 1). For example, the rapid vibration of the vocal folds modulates the airspace between them (i.e. the glottis) on the order of 100-400 cycles per second. When coupled with respiratory pressure the modulated glottis generates a train of flow pulses that, along with possible turbulence, will excite the acoustic resonances of the trachea, vocal tract, and nasal passages resulting in an acoustic wave radiated at the lips. Simultaneous, but much slower articulatory movements can be executed to modulate the shape of the pharyngeal and oral cavities, the coupling to the nasal system, the space between the vocal folds by abduction, or the magnitude of respiratory pressure. These slow modulations will shift the acoustic resonances up or down in frequency and valve the flow of air through the system, thus altering the characteristics of the radiated acoustic wave over time, and providing the stimulus from which listeners can extract phonetic information.

The purpose of this article is to demonstrate how a spoken phrase can be simulated with a model of speech production based on airway modulation. The input parameters impose time-dependent deformations on the airway shape which structure the acoustic signal into speech. Although this work is new in the sense of it being both theoretically and data-based, as well as implemented on a modern computer system, the interest in creating an artificial talker is centuries old. The aims of the article are to 1) provide a brief history of two artificial talking devices that were used in performance situations, 2) describe the background and main components of the airway modulation model, and 3) demonstrate how the model can be used to produce short phrases.
2. Abbreviated History of Talking Machines

Development of artificial talkers has long been of interest for purposes of science, technology, art, entertainment, and deception. The first true speaking machines are often attributed to Kratzenstein and von Kempelen[1, 2], both of whom built mechanical devices in which a sound source excited variously shaped resonant cavities resulting in speech-like sounds. Both also exhibited their inventions in the late 1700’s; Kratzenstein’s device, which could produce five vowels, won a prize in 1779 offered by the Imperial Academy of Sciences at St. Petersburgh. In the early 1800’s Charles Wheatstone [4] and Robert Willis [5] both attempted to recreate and improve upon von Kempelen’s speaking machine; in each case the primary interest was in acquiring a scientific understanding of speech production.

Perhaps no early inventor of artificial talkers exemplified the integration of engineering and theatrical presentation better than Joseph Faber. Although little is known about Faber’s personal life, according to Lindsay [6], he was born in Germany and first became an astronomer. His interests, however, eventually diverted into anatomy and mechanics. He supposedly began work on his speaking machine in the 1820’s, basing his design largely on von Kempelen’s published record of his device. A bellows supplied pressure to a reed which, in turn, supplied the acoustic excitation to a set of resonant chambers that could be coupled or decoupled with sliding plates. The components of the machine were controlled by levers connected to a keyboard and foot pedal. Thus, speech could be produced by hand and foot gestures of a trained operator (who apparently was Faber himself). After several years of demonstrating to European audiences that his invention (called the “Amazing Talking Machine”) could speak and sing with clarity, Faber traveled to New York City in 1844. The exhibitions there were met with mixed reviews. A newspaper correspondent was impressed enough to write that the only problem with the device was that it had “a strong German accent” [6], although interest from the general public was reportedly low.

Faber’s talking machine did, however, attract the attention of Princeton scientist Joseph Henry[2] who requested a private demonstration. Afterward Henry wrote to a colleague that “The plan of the machine is the same as that of the human organs of speech, the several parts being worked by strings and levers instead of tendons and muscles.” He also noted that “The German [i.e., Faber] was studying the

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1 It is possible, however, that these devices were preceded by a speaking machine designed by a French academian named Charles Sorel [3]. In the third volume of the 1667 edition of his textbook La Science Universelle, Sorel describes an intricate speaking machine consisting of pipes and a keyboard used to control their actions. He also wrote extensively about the “conjunction” of speech sounds as they were produced by the machine, which was apparently a precursor to the modern notion of articulation [3].

2 For whom the unit of electrical inductance is named.

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3 An acronym comprised of the capitalized letters in “Voice Operation DEmonstratoR.”
continued practice. Some twenty years after the World’s Fair exhibitions, one of the original trained operators was invited back to Bell Labs for an “encore performance” of sorts (the occasion was Homer Dudley’s retirement) with a restored version of the VODER. It was reported that “She sat down and gave a virtuoso performance...” [10].

The examples of both Faber’s Talking Machine and Dudley’s VODER, suggest that the operator of the device learns and internalizes a set of rules for generating speech with a new sound producing system. Although the ability of a human operator to acquire such rules is highly desirable for performance-driven artificial speech (or song), much research has been devoted to explicating those rules in an attempt to develop text-to-speech synthesis systems, as well as provide general knowledge about the speech planning and production process. A theoretical point of view concerning how such rules might be defined is to consider the speech signal as the result of multiple layers of modulation imposed on the underlying sound production device, whether it be of a mechanical, electrical, or biological nature. Indeed, based in part on the experience with the VODER, Dudley[12] expressed this view in an article called “The carrier nature of speech” by referring to the relatively high-frequency excitation provided by phonation or noise generation as “carrier waves” that are modulated by slowly-varying, and otherwise inaudible, movements of the vocal tract called “message waves.” He noted that this view applied across human speech, the VODER, and the vocoder system (and could be extended to apply to Faber’s talking machine as well.).

The subsequent sections of this article are intended to describe speech production in the framework of an airway modulation model. It will be shown that the “carrier nature of speech” perspective can be applied not just in terms of the excitation source and vocal tract movements, but at multiple levels of the speech production system. The primary purpose of this model is to facilitate understanding the acoustic characteristics of time-dependent changes in airway shape and ultimately how those characteristics are related to the perception of speech. The control parameters of the model, however, do lend themselves to real-time control, hence the model could potentially be configured as a performance-driven device.

### 3. Airway Modulation Model

The airway modulation model, also referred to as “Tube-Talker,” is a combination of two primary components: 1) a kinematic representation of the medial surfaces of the vocal folds, and 2) a kinematic area function representation of the trachea, nasal tract, and vocal tract airways. A multi-tier technique has been developed for controlling the model parameters in both components as is shown in Fig. 2. The leftmost column indicates quantities that define the basic physical structure of the system, the second column contains all the time-varying control parameters, the third column shows the covert intermediate quantities, and the rightmost column indicates the output quantities needed for sound production. Each tier will be described in the following sections.

#### 3.1. Kinematic model of the medial surfaces of the vocal folds

Modulation of the glottal airspace is accomplished with a kinematic representation of the vibrating portion of the vocal fold medial surfaces in which time-varying surface displacements are superimposed on a postural configuration [13, 14]. As can be seen in Fig. 3, the prephonatory posture is defined by superior (ξ̄₀) and inferior (ξ̄₁) values of separation at the vocal processes and by a bulging parameter (ξₖ) that provides curvature to the medial surface. The vocal fold length (antero-posterior dimension of the surface along midline) and thickness (inferior-superior extent of the surface) can be specified to be characteristic of a particular talker.

The time-varying (vibratory) displacement is based on a summation of translational and rotational modes in the vertical dimension and a ribbon mode in the antero-posterior dimension. The amplitude of vibration and mucosal wave velocity are governed by rules, as described in [14]. Any of the vibratory, aerodynamic, or structural parameters (e.g.,
fundamental freq. ($F_0$), bronchial pressure $P_b$, vocal process separation, etc.) can also be made to be time-varying as indicated in the “Tier 0” portion of Fig. 2. For example, the degree of separation of the vocal processes ($\xi_{02}$) could be increased to abduct the vocal folds for production of a voiceless consonant and then be reduced again for a voiced production. Thus, airway modulations produced at the level of the vocal folds operate on two time scales, one that is representative of their vibrational frequency (approximately 100-400 Hz) and another for the much slower adductory and abductory movements of the medial surfaces that take place during the unvoiced parts of speech.

The output of the kinematic source model is the glottal area function $a_g(t)$, calculated as the time-varying sum of the minimum area from each of the vertical channels of the medial surface. The glottal area is aerodynamically and acoustically coupled to a wave-reflection model of the trachea, vocal tract, and nasal tract [16, 17, 15]. The resulting glottal flow is determined by the interaction of the glottal area with the time-varying acoustic pressures present just inferior and superior to the glottis. A noise component is added to the glottal flow signal if the calculated Reynolds number within the glottis exceeds a threshold value (> 1200).

### 3.2. Kinematic model of the vocal tract area function

The vocal tract component of the model was described in Story[18] and is based on a perspective that vowels and vowel-to-vowel transitions are produced by modulating a phonetically-neutral vocal tract configuration. In turn, production of consonants results from another level of modulation that imposes severe constrictions on the underlying vowel or evolving vowel transition. This means that the length and other idiosyncratic features of the neutral vocal tract shape set the acoustic background on which vowel transitions are carried, while the vowel transitions provide the acoustic background on which consonant modulations are imposed. Thus, the neutral tract shape serves as a carrier for vowel modulations which, in turn, serve as a carrier for consonant constriction modulations.

The length and shape of the vocal tract is represented in the model by an area function. That is, the cross-sectional area variation along the long axis of the vocal tract is specified at discrete increments of length for a given instant of time. Based on the multi-tier approach previously developed for controlling the shape of the vocal tract[18], vowels are represented in Tier I (see Fig. 2) as modulations of an underlying neutral (in an acoustic sense) tract shape and consonants are imposed in Tier II as modulations of the underlying vowel substrate. Tier III allows for dynamic length change operations at both the glottal and lip ends, and nasal coupling is controlled by Tier IV.

In the first tier, vowel-to-vowel transitions $V(x, t)$ can be produced by perturbing a mean vocal tract configuration with two shaping patterns called modes such that,

$$V(x, t) = \frac{\pi}{4}(\Omega(x) + q_1(t)\phi_1(x) + q_2(t)\phi_2(x))^2 \tag{1}$$

where $x$ is the distance from the glottis and $\Omega(x)$, $\phi_1(x)$, and $\phi_2(x)$ are the mean vocal tract diameter function and modes, respectively, as defined in [18]. The time-dependence is produced by the mode scaling coefficients $q_1(t)$ and $q_2(t)$. The squaring operation and scaling factor of $\pi/4$ converts the diameters to areas.

Production of consonants are generated in Tier II with a scaling function $C(x)$ that extends along the length of the vocal tract. The value of $C(x)$ is equal to 1.0 everywhere except in the region of the desired constriction location $l_c$. The shaping of the constriction around $l_c$ is determined by a Gaussian function that includes control parameters for constriction extent along the tract length, and skewness. The extent $r_c$ is defined as the distance between the half maximum points of $C(x)$ and a skewing factor $s_c$ dictates the degree of asymmetry of the constriction. When any vowel-like area function is multiplied by $C(x)$, the region in the vicinity of $l_c$ will be reduced in area, thus superimposing the constriction. For velar consonants $r_c$ would typically be set to larger values to more accurately represent the extent of a constriction produced by the tongue body. The constriction function can be made time dependent with a temporal activation parameter called the consonant magnitude $m_c(t)$, such that it will impose the constriction to produce the specified cross-sectional area $a_c(t)$ at a specific time and location in the vocal tract.

A composite area function $A(x, t)$ is generated by the vocal tract model as the product of each element along the x-dimension of $V(x, t)$ and $C(x, t)$ such that at any given
primary consonant constrictions, and the temporal patterns of those same constrictions. At this point, such information is extracted from articulatory data collected with the University of Wisconsin-Madison’s X-ray microbeam system (XRMB) [19].

The first phrase simulated for this article was “The black cat” (broadly transcribed as /ðablækkæt/); this was chosen in part because it contains a variety of consonant types including a voiced fricative, bilabial, alveolar, and velar stops (both voiced and unvoiced), and a liquid. The XRMB system consists of tracking gold pellets affixed to the tongue, lips, and mandible during production of speech. Shown in Fig. 5a is the midsagittal configuration of the pellets at the first time frame in the phrase (i.e. during production of /ð/). The solid red points represent the actual pellet positions, whereas the open circles are phantom pellets that are an estimate of air tissue interface in the teeth and lip regions [20]. Most directly related to the TubeTalker model is the shape of the airspace itself. Based on the algorithm reported in [20], the airway shape in the oral cavity can be estimated by fitting a centerline and subsequently measuring the cross-distances at successive locations, anterior to posterior, from the lips toward the velar region. The cross-distance function for this time frame is shown in 5b. Performing this same analysis on each successive time frame over the duration of the utterance results in a time-varying cross-distance function, as plotted in Fig. 6, where the temporal and structural changes in oral cavity shape can be observed from left to right. Each of the consonant constrictions in the phrase are indicated by arrows.

The spatial location and temporal variation of both vowel and consonant components were determined based primarily on a technique reported in [21]. This technique first attempts to generate a best fit to the cross-distance in a given time frame, based on a linear combination of the modes and neutral vocal tract shape as presented previously in Eqn. 1, but configured for the XRMB data. When collected over all successive time frames of the phrase, this process produces the time-dependent coefficients, \( q_1(t) \) and \( q_2(t) \). These are

\[
A(x_i, t_n) = \prod_{i=1}^{N_x} V(x_i, t_n) C(x_i, t_n) \tag{2}
\]

where \( N_x \) is the number of cross-sectional areas representing the complete area function. All area functions used in the present study consisted of \( N_x = 44 \) contiguous “tubelet” sections as defined in [18]. An example area function is shown in Fig. 4. The glottis is located at the zero point along the x-axis, the tracheal area function extends from the glottis toward the bronchi in the negative x-direction, and the 44-section vocal tract extends toward the lips in the positive x-direction. The red line indicates the neutral area function \( \Omega(x) \), the blue line is a vowel modulation of the neutral shape based on Eqn. (1), and the black line demonstrates an area function with an occlusion located at the lips. The nasal coupling location is indicated by the upward pointing arrow located at about 8.8 cm from the glottis.

The TubeTalker model can potentially simulate any type of speech utterance if the appropriate information concerning the structure and timing of the input parameters is known. In the next section, simulation of two phrases is demonstrated based on extracting such information from articulatory data.

4. Simulation of phrase-level speech

Demonstrated in this section are the steps required to simulate a phrase with the TubeTalker model. The information needed in order to define the input parameters are the time-varying coefficients, \( q_1(t) \) and \( q_2(t) \), that define the vowel-to-vowel variation in Eqn. 1, the locations and extent of the

![Figure 4](image)

**Figure 4.** Demonstration of the area function model. The glottis is located at 0 cm, the trachea extends from the glottis in the negative direction and the vocal tract extends in the positive direction. The red line indicates the neutral area function \( \Omega(x) \), the blue line is a vowel modulation of the neutral shape based on Eqn. (1), and the black line demonstrates an area function with an occlusion located at the lips. The nasal coupling location is indicated by the upward pointing arrow located at about 8.8 cm from the glottis.

![Figure 5](image)

**Figure 5.** (a) Midsagittal representation of the \( \delta \) in “The black cat” based on articulatory data collected with the XRMB system. (b) Cross-distance function of the same time shown in (a).
plotted in the upper panel of Fig. 7a and indicate the vowel-to-vowel modulations that need to be imposed on the neutral vocal tract shape. The spatial location of each consonant constriction can be estimated directly from the cross-distance function, as indicated by the arrows. The temporal variation of each constriction (i.e., the onset, sustained portion, and offset) was determined from an error function based on the ratio of the original cross-distance function (Fig. 6) to a vowel-only version reconstructed with the \( q_1(t) \) and \( q_2(t) \) coefficients (see top panel, Fig. 7a). The timing functions for all the consonant constrictions in the phrase are shown together in second panel of Fig. 7a. The first three consonants are heavily overlapped in time, whereas the /k/ and /t/ are well separated from the other constrictions. The lower two panels indicate the time course of the nasal coupling area and the vocal fold separation distance (i.e., adduction/abduction), both of which have been determined by trial and error. For the “The black cat,” the nasal coupling is maintained at zero throughout, but the vocal folds need to move apart during the voiceless portions so that the vibration ceases and pressure builds up prior to the constriction release.

Shown in Fig. 8 is a time sequence of vocal tract area functions generated by the vowel and consonantal input parameters (upper two panels of Fig. 7b). The portion of the area functions extending from about 10-17.5 cm corresponds to the cross-distance function of the oral cavity plotted previously in Fig. 6; the constrictions are similarly located in space and time but the magnitudes appear somewhat different because this figure shows cross-sectional area rather than cross distance. Time-varying resonance frequencies (formants) calculated directly from two versions of the area function sequence are plotted in Fig. 7b. The blue lines indicate the formants that would exist in the absence of consonant constrictions (i.e., the case if all \( m_c(t) = 0 \)) and the red lines are those calculated when the constrictions are imposed.
imposed. The effect of modulating the vowel substrate provided by the Tier I parameters \(q_1(t)\) and \(q_2(t)\) with the constrictions generated by Tier II is a “deflection” of the formants away from their vowel-only paths, where the direction is determined by the location of the constriction along the vocal tract length.

The final step is to simulate the acoustic pressures and volume velocities as the vocal tract is modulated. The simulated acoustic waveform and corresponding wide-band spectrogram are shown in Fig. 9. The periods of silence or unvoiced sound are due to the increase in vocal fold separation that occurs at the beginning, at about 0.3-0.45 seconds, and at the end of the utterance. The periodic, but low-frequency portion that can be seen at about 0.1 seconds is due to acoustic radiation from the skin surfaces during the vocal tract occlusion for /b/.

For comparison, a second phrase was also simulated by the same methods described previously. The XRMV version of “The brown cow” (broadly transcribed as /ðbrəʊkɔ/)) was analyzed and the model input parameters determined. These are shown in Fig. 10a, where again there is temporal overlap of all parameters. In this case, there is also nasal coupling required during the production of the /n/, but must be brought to zero rapidly in order to adequately allow pressure to build up for the release of the velar /k/. The calculated formant frequencies for both the vowel-only and vowel+consonant cases are shown in Fig. 10b as the blue and red lines, respectively.

The simulated acoustic waveform for “The brown cow” is shown along with the corresponding wide-band spectrogram in Fig. 11.

5. Conclusion

An airway modulation model called TubeTalker was introduced as a system for generating artificial speech. The voice
source component is based on a kinematic representation of the medial vocal fold surfaces that can be set into vibration for voicing and abducted/adducted for voiceless portions of an utterance. The vocal tract is represented by an area function whose time-dependent shape is generated by vowel and consonant modulations. The result is a speech signal that can be analyzed in the same way as recorded, natural speech, and can be presented to listeners for formal or informal evaluation.

The model is currently implemented with a combination of code written in C and Matlab [22]. The vocal fold motion, flow calculations, and acoustic wave propagation are written in C and compiled as a Matlab mex file. Additional Matlab code is used to generate the time-varying area function and time-dependency of all parameters shown in Fig. 2. In its current form, the model runs with a compute-time to real-time ratio of about 8:1 on a PC laptop or Macbook Air, but it would possible to optimize the code for near real-time operation if desired.

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